

The DMC Contribution in the Human Absorption in an Indoor Environment

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Abstract—Room electromagnetics theory is applied to determine the influence of the diffuse multipath components (DMC) in the human specific absorption rate at 2.8 GHz. The whole-body absorption is determined for an exposure to a Line Of Sight (LOS) component plus the DMC.

Both experimental and numerical results show that the contribution of the DMC in the whole-body absorption can not be neglected. The whole-body specific absorption rate (SAR) may be due up to 90% to the DMC in an indoor environment.

I. INTRODUCTION

The International Commission on Non-Ionizing Radiation Protection (ICNIRP) [1] defines the Specific energy Absorption Rate (SAR) as a basic restriction for human exposure in the radio frequency (RF) band. Various works based on numerical computations such as the Finite-Difference Time-Domain (FDTD) method have assessed the SAR in phantoms [2]–[4], but the whole-body SAR has been calculated in these papers for a set of plane waves exposure.

The presence of the DMC is reported recently in [5], and it has gained interest in the wireless channels parameters estimators community. The characteristics of DMC in an indoor environment are investigated in [6], where it turns out that the contribution of the DMC to the total power may range from 10% to 95%. Hence, the DMC power may contribute to the absorption in human in a realistic environment. This matter is not yet addressed in the literature. The DMC contribution in the absorption is determined experimentally and afterwards numerically using Finite-Difference Time-Domain (FDTD) simulation. The outline of this abstract is as follows: In Section 2, we present the materials and the methods. Section 3 is devoted to the results from measurements and numerical computation. Conclusion is drawn in Section 4.

II. METHODS

A virtual Multiple Input Multiple Output (MIMO) channel sounder is used to probe the channel. For the present work, the Tx location is fixed and the Rx is

positioned at 100 (10×10) different locations forming a virtual uniform rectangular array. Both antennas are polarized vertically and positioned at a height of about 1.80 m above the ground. Five cylindrical phantoms in Polyvinyl chloride (PVC) (height = 150 cm, diameter = 24 cm) are used to assess the absorption cross section of one phantom (ACS). Phantoms were filled with water with following properties: $\sigma=1.58 \Omega^{-1}/\text{m}$ (conductivity), $\epsilon_r=77.32$ (relative permittivity) and $\rho=1000 \text{ kg/m}^3$ (mass density). The measurements are performed in an office room of about 360 m^3 .

Experimentally, the SAR_{wb}^{meas} of the phantom is determined from its absorption cross section (ACS in m^2) and the incident power densities, i.e., line of sight (LOS) and DMC (in W/m^2). Room electromagnetics theory is applied in [7] to assess the ACS of humans. The same method is used here for the ACS assessment of the phantom. Since the LOS component amplitude is measured, its power density is easily determined [8], [9] and the DMC power density is investigated in [10]. As already stated, the contribution of the DMC power density in the total power may vary drastically. Fig. 1 shows the relation between the LOS and DMC power densities in our investigated indoor environment [9]. The SAR_{wb} is calculated for 3 scenarios:

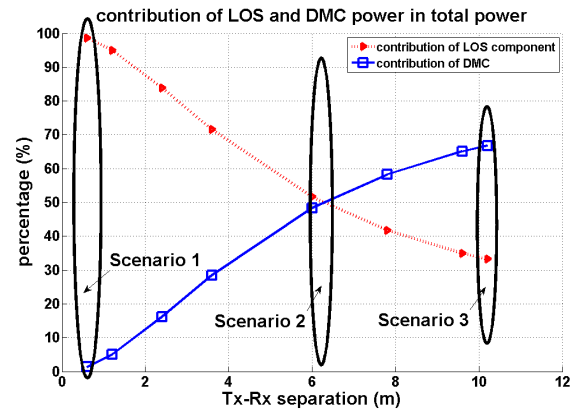


Fig. 1. Contribution of coherent and DMC in the total power density in the investigated room

- 1) the phantom is in the vicinity of the transmitter, i.e., where the LOS component is dominating
- 2) the phantom is located at the reverberation distance (where the LOS and the DMC power densities are the same, about 6 m in Fig. 1)
- 3) the phantom is far away from the transmitter, i.e., where the LOS component can be neglected compared to the DMC component

The experimentally measured whole-body SAR is expressed as follows:

$$SAR_{wb}^{meas} = SAR_{wb}^{spec} + SAR_{wb}^{dif}$$

$$= \frac{ACS}{m} (I_{dif} + \frac{1}{\pi} \sum_{k=1}^{N_{sc}} I_{sc}^k) \quad (1)$$

where SAR_{wb}^{spec} , SAR_{wb}^{dif} , I_{dif} , I_{sc}^k , N_{sc} represent the absorption rate due to the specular components, the absorption rate due to the DMC, the total power density of the DMC, the power density of the k^{th} specular path and the total number of specular paths, respectively. Note that for this work, only the first specular component (LOS) is taken into account ($N_{sc}=1$). For the numerical calculations, the FDTD method (SEMCAD-X [11]) has been used to compute the averaged SAR_{wb}^{fdd} absorbed by the phantom. The same dielectric properties are used during the simulations. The DMC are modeled with plane waves in SEMCAD-X as follows: an exponential decay, a white azimuthal spectrum, uniformly distributed delays in time domain, an elevation in the horizontal plane ($\theta=90^\circ$). The power densities (in mW/m²) used are summarized in Table. I.

Phantom-Tx	LOS power	DMC power	Total power
0.60 m (scenario 1)	694.40	2.90	697.30
6 m (scenario 2)	2.20	2.1	4.30
10.20 m (scenario 3)	0.40	1.60	2

TABLE I
POWER DENSITIES ACCORDING TO THE SCENARIOS

III. RESULTS

Table II shows the experimentally measured SAR_{wb} values and the percentage of the DMC contribution. It can be seen that in the vicinity of the transmitter (scenario 1) the highest power density leads to the highest absorption rate. As the phantom is moved away from the transmitter, the SAR_{wb}^{meas} decreases drastically. Even though the absorption decreases with increasing separation from the transmitter, the contribution of the DMC becomes more significant, varying from 1.30% (scenario 1) up to 92% (scenario 3). For the numerical simulation the DMC is modeled with 0, 4, 8, 16, 32, 64 and 72 plane waves to show

	scenario 1	scenario 2	scenario 3
SAR_{wb}^{meas}	1284.30 (μ W/kg)	16.10 (μ W/kg)	9.90 (μ W/kg)
Part of DMC in SAR_{wb}^{meas}	1.30 %	75 %	92.60 %

TABLE II
 SAR_{wb}^{meas} FOR DIFFERENT SCENARIOS

	DMC (no. of plane waves)	0	4	8	16	32	64	72
Scenario 1	SAR_{wb}^{fdd} (μ W/kg)	668	723	717	705	707	718	720
	DMC contribution (%)	0	7.6	6.8	5.2	5.5	6.9	7.3
	ΔSAR_{wb} (dB)	2.8	2.5	2.5	2.6	2.6	2.5	2.5
Scenario 2	SAR_{wb}^{fdd} (μ W/kg)	2.1	7.1	6.9	6.1	8.3	13	14.2
	DMC contribution (%)	0	35.1	33.8	28.5	43.7	76.9	85
	ΔSAR_{wb} (dB)	2.7	3.6	3.7	4.2	2.9	0.9	0.6
Scenario 3	SAR_{wb}^{fdd} (μ W/kg)	0.4	3.2	3.2	2.8	4.5	8	8.8
	DMC contribution (%)	0	32	31.7	27.6	46.1	85.7	95.7
	ΔSAR_{wb} (dB)	2.6	4.9	4.9	5.4	3.7	0.9	0.5

TABLE III
 SAR_{wb}^{fdd} FOR THE THREE SCENARIOS

convergence and accuracy of the modeling. Table III lists the numerical results where the values in bold are the most accurate. Unfortunately, simulating with more plane waves was not possible, because of software and/or hardware limitations. Moreover Table III shows that from 64 planes waves on the results do not vary much and 72 planes waves satisfy.

ΔSAR_{wb} is the relative error (in dB) between the experimentally measured SAR_{wb} and the simulated SAR_{wb} . The DMC contribution varies from 1.3% to 92% in the experimental SAR whereas it varies from 7.3% up to 95.7% for the numerical calculation, indicating the importance of the DMC in the total absorption. In the full paper, the methods and the results will be discussed in details.

IV. CONCLUSION

The DMC contribution in the whole-body specific absorption rate is studied in this paper. Even though the whole-body SAR_{wb} decreases with increasing separation from the transmitter, the contribution of the DMC in the absorption may reach up to 90%. Experimental and numerical results agree very well as long as the plane wave assumption is valid (scenario 2 and 3). Checking compliance with the ICNIRP guidelines is not the purpose of the present paper, but the presented method can be used for this. We present a method to determine experimentally the whole-body SAR in real environments plus its validation via numerical simulations. In addition, the DMC contribution is highlighted. Comparison with the ICNIRP restrictions values requires also the knowledge of the duty cycle of the considering system.

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